

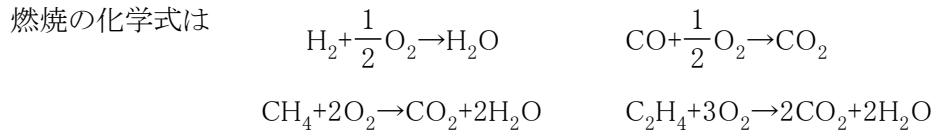
## ＜燃焼後のガス量と組成＞

気体燃料の組成

名前	%
水素	50
一酸化炭素	9
メタン	26
エチレン	4
酸素	0.1
窒素	8
二酸化炭素	2.5
水蒸気	0.4

この表の組成の気体燃料1m<sup>3</sup><sub>N</sub>を燃焼させたときの理論酸素量、理論空気量、供給した燃焼用空気量、燃焼ガス量と組成を求める。

空気過剰率  $\lambda = 1.4$  とする



$$\begin{aligned} \text{理論酸素量} &= \frac{1}{2} \times \text{水素} + \frac{1}{2} \times \text{一酸化炭素} + 2 \times \text{メタン} + 3 \times \text{エチレン} - \text{酸素} \\ &= \frac{1}{2} \times 0.5[\text{m}^3] + \frac{1}{2} \times 0.09[\text{m}^3] + 2 \times 0.26[\text{m}^3] + 3 \times 0.04[\text{m}^3] - 0.001[\text{m}^3] = 0.934[\text{m}^3] \end{aligned}$$

空気中の酸素は21%とすると

$$\text{理論空気量} = \text{理論酸素量} \times \frac{1}{0.21} = 0.934[\text{m}^3] \times \frac{100}{21} = 4.448[\text{m}^3]$$

$$\text{供給した燃焼用空気量} = \text{理論空気量} \times \lambda = 4.448[\text{m}^3] \times 1.4 = 6.227[\text{m}^3]$$

湿り燃焼ガス量

$$\begin{aligned} &= \text{供給した燃焼用空気量} + 1[\text{m}^3] - \text{理論酸素量} + 2 \times \text{メタン} + 3 \times \text{エチレン} \\ &= 6.227[\text{m}^3] + 1[\text{m}^3] - 0.934[\text{m}^3] + 2 \times 0.26[\text{m}^3] + 3 \times 0.04[\text{m}^3] = 6.933[\text{m}^3] \end{aligned}$$

乾き燃焼ガス量

$$\begin{aligned} &= \text{供給した燃焼用空気量} + 1[\text{m}^3] - \text{理論酸素量} + \text{エチレン} - \text{水素} \\ &= 6.227[\text{m}^3] + 1[\text{m}^3] - 0.934[\text{m}^3] + 0.04[\text{m}^3] - 0.5[\text{m}^3] = 5.833[\text{m}^3] \end{aligned}$$

$$\text{燃焼生成水蒸気量} = \text{湿り燃焼ガス量} - \text{乾き燃焼ガス量} = 6.933[\text{m}^3] - 5.833[\text{m}^3] = 1.1[\text{m}^3]$$

燃焼ガスの組成を求めていく。次の表に入れる。

燃焼ガスの組成

名前	%
O <sub>2</sub>	5.4
CO <sub>2</sub>	6.6
N <sub>2</sub>	72.1
H <sub>2</sub> O	15.9
計	100

O<sub>2</sub>の割合

$$\text{燃焼後の酸素の量} = \text{理論空気量} \times (\lambda - 1) \times 0.21 = 4.448[\text{m}^3] \times (1.4 - 1) \times 0.21 = 0.374[\text{m}^3]$$

$$\text{燃焼ガスの組成}_{\text{O}_2} = \frac{\text{燃焼後の酸素の量}}{\text{湿り燃焼ガス量}} \times 100 = \frac{0.374[\text{m}^3]}{6.933[\text{m}^3]} \times 100 = 5.4$$

## CO<sub>2</sub>の割合

$$\begin{aligned} \text{燃焼後の二酸化炭素の量} &= \text{一酸化炭素} + \text{メタン} + 2 \times \text{エチレン} + \text{二酸化炭素} \\ &= 0.09[\text{m}^3] + 0.26[\text{m}^3] + 2 \times 0.04[\text{m}^3] + 0.025[\text{m}^3] = 0.455[\text{m}^3] \end{aligned}$$

$$\begin{aligned} \text{燃焼ガスの組成}_{2,3} &= \text{燃焼後の二酸化炭素の量} / \text{湿り燃焼ガス量} \times 100 \\ &= 0.455[\text{m}^3] / 6.933[\text{m}^3] \times 100 = 6.6 \end{aligned}$$

## N<sub>2</sub>の割合

$$\begin{aligned} \text{燃焼後の窒素の量} &= \text{供給した燃焼用空気量} \times 0.79 + 0.08[\text{m}^3] \\ &= 6.227[\text{m}^3] \times 0.79 + 0.08[\text{m}^3] = 4.999[\text{m}^3] \end{aligned}$$

$$\text{燃焼ガスの組成}_{2,4} = \text{燃焼後の窒素の量} / \text{湿り燃焼ガス量} \times 100 = 4.999[\text{m}^3] / 6.933[\text{m}^3] \times 100 = 72.1$$

## H<sub>2</sub>Oの割合

$$\begin{aligned} \text{燃焼後の水蒸気の量} &= \text{水素} + 2 \times \text{メタン} + 2 \times \text{エチレン} + \text{水蒸気} \\ &= 0.5[\text{m}^3] + 2 \times 0.26[\text{m}^3] + 2 \times 0.04[\text{m}^3] + 0.004[\text{m}^3] = 1.104[\text{m}^3] \end{aligned}$$

$$\begin{aligned} \text{燃焼ガスの組成}_{2,5} &= \text{燃焼後の水蒸気の量} / \text{湿り燃焼ガス量} \times 100 \\ &= 1.104[\text{m}^3] / 6.933[\text{m}^3] \times 100 = 15.9 \end{aligned}$$

## 理論燃焼温度を求める

燃料温度100℃、余熱空気温度300℃、空気温度30℃のとき空気過剰率1.0～1.5に対する理論燃焼温度を求める

### 燃料の低発熱量

$$\begin{aligned} &= \text{水素の低発熱量} \times \text{水素} + \text{一酸化炭素の低発熱量} \times \text{一酸化炭素} + \text{メタンの低発熱量} \times \text{メタン} \\ &+ \text{エチレンの低発熱量} \times \text{エチレン} \\ &= 10800[\text{kJ}/\text{m}^3] \times 0.5[\text{m}^3] + 12700[\text{kJ}/\text{m}^3] \times 0.09[\text{m}^3] + 35900[\text{kJ}/\text{m}^3] \times 0.26[\text{m}^3] \\ &+ 59900[\text{kJ}/\text{m}^3] \times 0.04[\text{m}^3] = 18273[\text{kJ}] \end{aligned}$$

### 燃料の熱量

$$\begin{aligned} &= (1.292[\text{kJ}/\text{m}^3\text{K}] \times \text{水素} + 1.301[\text{kJ}/\text{m}^3\text{K}] \times \text{一酸化炭素} + 1.652[\text{kJ}/\text{m}^3\text{K}] \times \text{メタン} \\ &+ 2.105[\text{kJ}/\text{m}^3\text{K}] \times \text{エチレン} + 1.319[\text{kJ}/\text{m}^3\text{K}] \times \text{酸素} + 1.306[\text{kJ}/\text{m}^3\text{K}] \times \text{窒素} \\ &+ 1.725[\text{kJ}/\text{m}^3\text{K}] \times \text{二酸化炭素} + 1.499[\text{kJ}/\text{m}^3\text{K}] \times \text{水蒸気}) \times 100[^\circ\text{C}] \\ &= 534.0[\text{kJ}] \end{aligned}$$

### 供給された空気の熱量(λ)

$$= \text{理論空気量} \times \lambda \times (0.21 \times 1.356[\text{kJ}/\text{m}^3\text{K}] + 0.79 \times 1.314[\text{kJ}/\text{m}^3\text{K}]) \times 300[^\circ\text{C}]$$

## t℃のときの燃焼後のガスの熱量

$$\begin{aligned} &= \text{比熱}(t,1) \times \text{燃焼後の酸素の量} + \text{比熱}(t,2) \times \text{燃焼後の窒素の量} \\ &+ \text{比熱}(t,3) \times \text{燃焼後の二酸化炭素の量} + \text{比熱}(t,4) \times \text{燃焼後の水蒸気の量} \end{aligned}$$

### 燃焼後のガスの熱量(λ,t)

$$\begin{aligned} &= \text{比熱}(t,1) \times \text{理論空気量} \times (\lambda - 1) \times 0.21 + \text{比熱}(t,2) \times (\text{理論空気量} \times \lambda \times 0.79 + 0.08[\text{m}^3]) \\ &+ \text{比熱}(t,3) \times 0.455[\text{m}^3] + \text{比熱}(t,4) \times 1.103[\text{m}^3] \end{aligned}$$

$$t_{\text{new}}(\lambda, t) = \frac{\text{燃料の低発熱量} + \text{燃料の熱量} + \text{供給された空気の熱量}(\lambda)}{\text{燃焼後のガスの熱量}(\lambda, t)} - 273.15$$

平均定圧比熱

温度℃	O <sub>2</sub>	N <sub>2</sub>	CO <sub>2</sub>	H <sub>2</sub> O	H <sub>2</sub>	CO	CH <sub>4</sub>	C <sub>2</sub> H <sub>4</sub>
0	1.306	1.302	1.620	1.490	1.277	1.299	1.544	1.871
100	1.319	1.306	1.725	1.499	1.292	1.301	1.652	2.105
200	1.335	1.310	1.775	1.520	1.290	1.307	1.765	2.327
300	1.356	1.314	1.892	1.545	1.300	1.316	1.890	2.530
400	1.381	1.327	1.955	1.557	1.303	1.329	2.019	2.720
500	1.402	1.335	2.022	1.582	1.305	1.342	2.143	2.892
600	1.419	1.348	2.070	1.607	1.308	1.357	2.263	3.049
700	1.436	1.360	2.122	1.633	1.312	1.372	2.381	3.189
800	1.453	1.373	2.164	1.662	1.317	1.386	2.489	3.342
900	1.469	1.386	2.202	1.691	1.323	1.399	2.590	3.447
1000	1.482	1.398	2.235	1.716	1.329	1.412	2.689	3.562
1100	1.490	1.411	2.265	1.741	1.336	1.424	2.780	
1200	1.503	1.423	2.294	1.766	1.344	1.436	2.862	
1300	1.511	1.432	2.315	1.792	1.352	1.446		
1400	1.524	1.444	2.340	1.817	1.360	1.456		
1500	1.532	1.453	2.361	1.838	1.368	1.465		
1600	1.540	1.461	2.382	1.863	1.376	1.474		
1700	1.549	1.469	2.399	1.884	1.385	1.482		
1800	1.557	1.478	2.415	1.905	1.393	1.490		
1900	1.566	1.482	2.428	1.925	1.401	1.497		
2000	1.574	1.490	2.445	1.946	1.409	1.503		
2100	1.578	1.500	2.457	1.967	1.417	1.510		
2200	1.586	1.503	2.470	1.984	1.425	1.516		
2300	1.595	1.511	2.482	2.001	1.433	1.521		
2400	1.599	1.515	2.491	2.018	1.440	1.526		
2500	1.607	1.520	2.499	2.030	1.448	1.531		
2600	1.612	1.528	2.507	2.047	1.455	1.537		
2700	1.616	1.532	2.520	2.060	1.462	1.541		
2800	1.624	1.536	2.528	2.076	1.469	1.545		
2900	1.628	1.540	2.537	2.089	1.476	1.549		
3000	1.637	1.545	2.541	2.097	1.482	1.533		

```

比熱(x,y)
xi=[x/100]
CpDown=平均定圧比熱y+1,xi+2
CpUp=平均定圧比熱y+1,xi+3
return (CpDown+(CpUp-CpDown)(x/100-xi))[kJ/m³]
    
```

理論燃焼温度<sub>1..6</sub>=0      空気過剰率<sub>1..6</sub>=0

```

( for k = 1 to 6 step 1 )
λ = 1 + 0.1(k-1)
空気過剰率k = λ
t = 2000
( ( for j = 1 to 100 step 1 )
t2 = t_new( λ , t )
break |t2-t| < 0.1
)
t = t2
理論燃焼温度k = t
    
```

理論燃焼温度={2262, 2131, 2019, 1921, 1830, 1750}

グラフを描く      { 空気過剰率, 理論燃焼温度 }

カルキングのデータグラフで作成

